

## PERFORMANCE OF THE DOUBLE SAMPLING NP CHART BASED ON THE MEDIAN RUN LENGTH

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**ABSTRACT.** **Objectives:** The purpose of this study is to use the median run length (MRL) as a criterion to measure the performance of the double sampling (DS)  $np$  chart. **Methods/statistical analysis:** An optimization model of the DS  $np$  chart is developed in this study by minimizing the out-of-control MRL. **Findings:** The numerical and graphical results show that the shape of the run length distribution of the DS  $np$  chart changes in accordance to the magnitude of shift in the process fraction nonconforming, from highly skewed when there is no process shift to almost symmetric when the process shift is large. The existing DS  $np$  chart is evaluated based on the average run length (ARL) criterion. However, the ARL does not provide a clear picture about the chart's performance when the run length distribution is skewed. Herein, we recommend an optimal design of the MRL-based DS  $np$  chart which delivers a better interpretation for the performance of the DS  $np$  chart. **Application/Improvements:** The optimal parameters of the MRL-based DS  $np$  chart are provided in this study.

### 1. INTRODUCTION

The double sampling (DS) method proposed by [1] was claimed as economically better than the single sampling method. Research on the DS method was gaining interest among researchers as some of the properties of the DS chart are superior to the competing charts [2]. The DS  $np$  chart was proposed by [3] and

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2010 *Mathematics Subject Classification.* 62P30, 49M37.

*Key words and phrases.* average run length, double sampling  $np$  chart, median run length.

the DS  $np$  chart was compared with the single-sampling  $np$  chart, the variable sample size  $np$  chart, the CUSUM  $np$  chart and the EWMA  $np$  chart. The comparison showed that the DS  $np$  chart is the quickest control chart to detect the increasing shift in the process fraction nonconforming.

The average run length (ARL) has been widely used as the performance measure of the control charts over the past few decades. The ARL is the average number of samples plotted on the control chart before an out-of-control signal is triggered. However, many researchers questioned the sole dependence on the ARL as a criterion to measure the chart's performance, such as [4–6]. On the other hand, the median run length (MRL) is a better criterion to interpret the chart's performance compared to the ARL when the run length distribution is skewed (see [4, 5]), where the MRL is the 50th percentile of the run length distribution. As pointed out by [6], the percentiles of the run length distribution including the MRL provide a better indication of the chart's performance. Noted by [5], the use of the MRL develops quality practitioners' confidence to have a better understanding of the performance of a control chart. In view of this advantage, the MRL is proposed as the performance measure to design the control charts by researchers such as [7, 8], to name a few.

The DS  $np$  chart proposed by [3] was evaluated based on the ARL criterion. However, the ARL is the average of the run length (RL) that has been reported to be inappropriate in representing “half of the time” [9] and hence quality practitioners should refrain from taking this approach. Consequently, the MRL-based DS  $np$  chart is proposed in this study, where the MRL is suggested as an alternative criterion to evaluate the performance of the DS  $np$  chart. The main contributions of this study are: (1) to provide a procedure to design the MRL-based DS  $np$  chart for the process fraction nonconforming, and (2) to provide the optimal parameters for the MRL-based DS  $np$  chart.

## 2. A REVIEW OF THE DS NP CHART

**2.1. The DS  $np$  Chart.** The DS  $np$  chart proposed by [3] was employed to monitor the quality characteristic of a process, which is the number of nonconforming items in a sample and it is assumed that the underlying process follows a binomial distribution.

The operation procedure of the DS  $np$  chart is outlined as follows:

- Step 1. The chart limits are set as  $WL = Ac_1 + 0.5$ ,  $CL_1 = Re - 0.5$  and  $CL_2 = Ac_2 + 0.5$ , where  $WL$ ,  $CL_1$  and  $CL_2$  are the warning limit for the first stage of the DS scheme, the control limit for the first stage of the DS scheme and the control limit for the second stage of the DS scheme, respectively. In these expressions,  $Ac_1$ ,  $Re_1$  and  $Ac_2$  are the acceptance number in the first sample, the rejection number in the first sample and the acceptance number in the second stage, respectively.
- Step 2. A sample of size  $n_1$  is taken and the number of nonconforming items  $d_1$  in this first sample is counted, in which the procedure is at the first stage of the DS scheme.
- Step 3. (a) If  $d_1 < WL$ , the process is considered as in- control and return to Step 2.  
 (b) If  $d_1 > CL_1$ , the process is concluded to be out-of-control and a corrective action is taken to search and remove the assignable cause(s), then return to Step 2.  
 (c) If  $WL < d_1 < CL_1$ , the process is considered as in-control and the procedure goes to the second stage of the DS scheme, in which a second sample of size  $n_2$  is taken and the number of nonconforming items  $d_2$  in this second sample is counted. After that, proceed to the next step.
- Step 4. If  $(d_1 + d_2) < CL_2$ , the process is concluded to be in-control and return to Step 2. Otherwise, the process is concluded as out-of-control and a corrective action is taken to search and remove the assignable cause(s), then return to Step 2.

Let  $\lfloor \cdot \rfloor$  and  $\lceil \cdot \rceil$  denote the round down and round up to the nearest integer, respectively. The probability of a plotted sample falling within the chart limits of the DS  $np$  chart [3] is given by

$$(2.1) \quad A = A_1 + A_2,$$

where

$$(2.2) \quad \begin{aligned} A_1 &= P(d_1 \leq \lfloor WL \rfloor) \\ &= \sum_{d_1=0}^{\lfloor WL \rfloor} C_{d_1}^{n_1} p^{d_1} (1-p)^{n_1-d_1} \end{aligned}$$

and

$$\begin{aligned}
 A_2 &= P([WL] < d_1 < [CL_1]) \cap P(d_1 + d_2 \leq [CL_2]) \\
 (2.3) \quad &= \sum_{d_1=[WL]+1}^{[CL_1]-1} \left[ C_{d_1}^{n_1} p^{d_1} (1-p)^{n_1-d_1} \left( \sum_{d_2=0}^{[CL_2]-d_1} C_{d_2}^{n_2} p^{d_2} (1-p)^{n_2-d_2} \right) \right].
 \end{aligned}$$

Here,  $C_d^n = \frac{n!}{d!(n-d)!}$ . Note that  $A_1$  is the probability that  $d_1 < WL$  at the first stage of the DS scheme, while  $A_2$  is the probability that  $WL < d_1 < CL_1$  at the first stage of the DS scheme and  $(d_1 + d_2) < CL_2$  at the second stage of the DS scheme.

The efficiency of the DS  $np$  chart is determined by its speed in detecting an increasing shift in the process fraction nonconforming  $p$  with the magnitude of shift  $\delta = p_1/p_0$ , where  $p_1 > p_0$ . Note that  $p = p_0$  when  $\delta = 1$ , while  $p = p_1$  when  $\delta > 1$ . Here,  $p_0$  is the in-control fraction nonconforming and  $p_1$  is the out-of-control fraction nonconforming.

**2.2. The Run Length Properties.** Since the RL of the control chart is geometric distributed, the probability mass function (pmf) and the cumulative distribution function (cdf) of the RL in general [10] are defined as

$$(2.4) \quad f_{RL}(l) = (1 - A)A^{l-1}$$

and

$$(2.5) \quad F_{RL}(l) = P(RL \leq l) = 1 - A^l,$$

respectively, for  $l = 1, 2, 3, \dots$ . Using the cdf in (2.5), [6] presented a simplified method, in which the  $100\alpha$ th ( $0 < \alpha < 1$ ) percentile of the RL can be computed as the smallest integer  $\tau$  such that

$$(2.6) \quad \tau \geq \frac{\ln(1 - \alpha)}{\ln A}.$$

This enables the percentile value to be computed easily. Since the MRL is the smallest RL with a cumulative probability of at least 50% of the time, then  $\alpha = 0.5$  in (2.6). Note that  $MRL = MRL_0$  is the in-control MRL when  $\delta = 1$ , whereas  $MRL = MRL_1$  is the out-of-control MRL when  $\delta > 1$ .

As suggested by [3], the average sample size of the DS  $np$  chart is computed as

$$(2.7) \quad ASS = n_1 + n_2 A_r,$$

where  $A_r = P(\lfloor WL \rfloor < d_1 < \lceil CL_1 \rceil)$  is the probability of taking the second sample of size  $n_2$ . Two ASS values are usually of interest, namely the in-control ASS ( $ASS_0$ ) and the out-of-control ASS ( $ASS_1$ ).

### 3. OPTIMAL DESIGN OF THE DS NP CHART BASED ON THE MRL

An optimization model of the DS  $np$  chart based on the MRL is developed in this section by minimizing the objective function which is expressed as

$$(3.1) \quad \min_{n_1, n_2, WL, CL_1, CL_2} MRL_1(\delta_{opt})$$

subject to

$$(3.2) \quad MRL_0 \geq MRL_{0\min},$$

$$(3.3) \quad ASS_0 = n,$$

$$(3.4) \quad 1 \leq n_1 < n < n_1 + n_2 \text{ and } n_1 < n_2,$$

where  $MRL_1(\delta_{opt})$  is the  $MRL_1$  value at the desired shift size  $\delta_{opt}$  in the process fraction nonconforming  $p$  for a fast detection,  $MRL_{0\min}$  is the minimum desired  $MRL_0$  and  $n$  is the desired  $ASS_0$ .

A control chart is considered superior to its competitors if this control chart gives the smallest  $MRL_1$  value. Similarly, when designing the DS  $np$  chart at a desired shift, the parameters that produce the lowest  $MRL_1$  are identified as the optimal parameters from all the possible  $(n_1, n_2, WL, CL_1, CL_2)$  combinations. The optimization procedure is detailed below:

- Step 1. Specify the desired values of  $MRL_{0\min}$ ,  $\delta_{opt}$ ,  $p_0$  and  $n$ .
- Step 2. All possible pairs of  $(n_1, n_2)$  are selected based on the constraints in (3.4). For each pair of  $(n_1, n_2)$ , the  $CL_1$  value is determined for any fixed value of  $WL$ , then the  $CL_2$  value is determined for any fixed values of  $WL$  and  $CL_1$ . Here, the values of  $WL$ ,  $CL_1$  and  $CL_2$  are adjusted such that  $MRL_0 \geq MRL_{0\min}$  and  $ASS_0 = n$ . The values of  $WL$ ,  $CL_1$  and  $CL_2$  are determined based on Step 1 of the operation procedure discussed in previous section, where  $0 < WL < CL_1 \leq CL_2$ . Therefore, we can obtain all the possible  $(n_1, n_2, WL, CL_1, CL_2)$  combinations that satisfy the constraints in (3.2) – (3.4).

Step 3. For each possible  $(n_1, n_2, WL, CL_1, CL_2)$  combination in Step 2, compute the  $MRL_1$  by means of (2.6) (when  $p = p_1$  and  $\alpha = 0.5$ ) and search for the optimal  $(n_1, n_2, WL, CL_1, CL_2)$  combination with the lowest  $MRL_1(\delta_{opt})$  value. Since the  $MRL$  is an integer, it can be happened that more than one optimal  $(n_1, n_2, WL, CL_1, CL_2)$  combinations that produce the similar lowest  $MRL_1(\delta_{opt})$  value. For such a case, the optimal  $(n_1, n_2, WL, CL_1, CL_2)$  combination that delivers the lowest  $ASS_1$  value is selected as the optimal parameter combination of the DS  $np$  chart.

An optimization MATLAB program is written by incorporating the aforementioned three-step procedure to compute the optimal  $(n_1, n_2, WL, CL_1, CL_2)$  combination for the DS  $np$  chart.

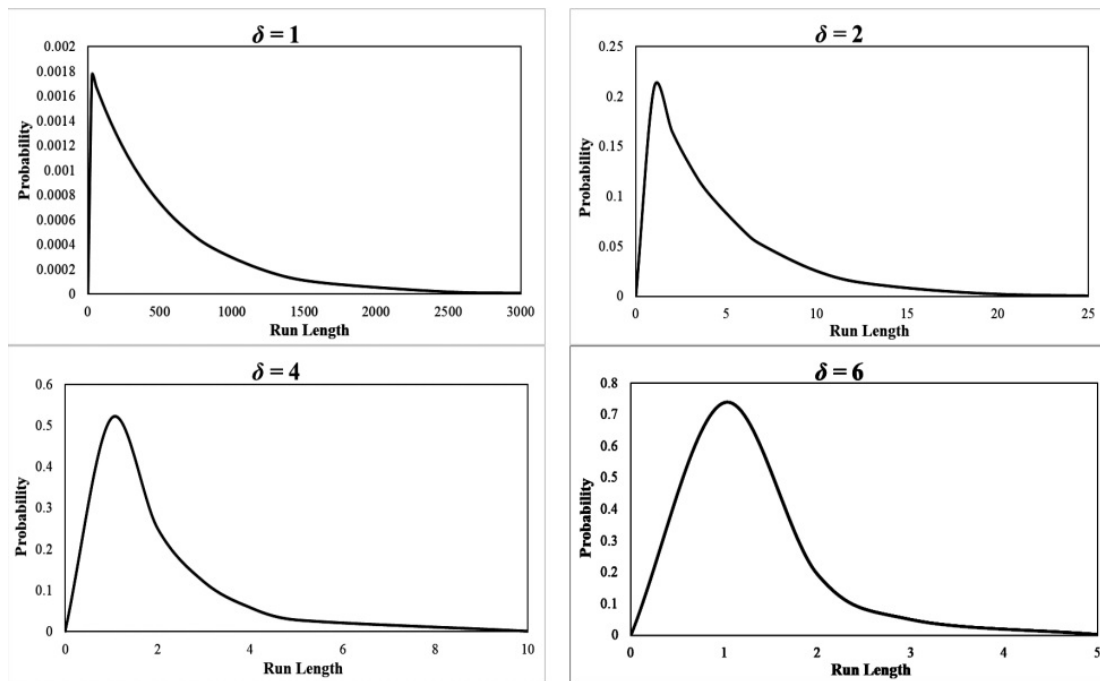


FIGURE 1. Plots of the pmf of the RL for the DS  $np$  chart with  $(n_1, n_2, WL, CL_1, CL_2) = (43, 2276, 1.5, 5.5, 34.5)$  when  $\delta_{opt} = 1.5$ ,  $p_0 = 0.01$ ,  $n = 200$  and  $MRL_{0min} = 370.4$  for various shift sizes in  $p$

#### 4. PERFORMANCE OF THE DS NP CHART BASED ON THE MRL

The plots of the pmf of the RL for the DS  $np$  chart in Figure 1 are obtained by considering  $(n_1, n_2, WL, CL_1, CL_2) = (43, 2276, 1.5, 5.5, 34.5)$  for  $\delta_{opt} = 1.5$ ,  $n = 200$ ,  $p_0 = 0.01$  and  $MRL_{0\min} = 370.4$ . As demonstrated in Figure 1, the skewness of the RL distribution of the DS  $np$  chart changes from highly right skewed when there is no shift ( $\delta = 1$ ) to almost symmetric for the large shift size.

In this study, the DS  $np$  chart is optimally designed based on the  $MRL$ , where the  $MRL$  values are computed by assuming that the underlying process follows a binomial distribution. The optimal  $(n_1, n_2, WL, CL_1, CL_2)$  combination of the DS  $np$  chart as well as the corresponding  $MRL_0$  and  $ARL_0$  values are presented in Table 1 with  $MRL_{0\min} \in \{200, 370.4\}$ ,  $\delta_{opt} \in \{1.5, 2, 3\}$ ,  $p_0 \in \{0.005, 0.01, 0.02\}$  and  $n \in \{25, 50, 100, 200, 400, 800\}$ . These optimal  $(n_1, n_2, WL, CL_1, CL_2)$  combinations will facilitate quality practitioners to choose the optimal parameters of the  $MRL$ -based DS  $np$  chart in the implementation of the DS  $np$  chart. For example, when  $\delta_{opt} = 2$ ,  $MRL_{0\min} = 200$ ,  $p_0 = 0.02$  and  $n = 50$ , the optimal  $(n_1, n_2, WL, CL_1, CL_2)$  combination is  $(25, 282, 1.5, 4.5, 12.5)$ . In addition, Table 1 provides a comparison between the  $ARL_0$  and  $MRL_0$  values of the DS  $np$  chart. It is noted that all the  $MRL_0$  values are smaller than the corresponding  $ARL_0$  values.

#### 5. THE PERFORMANCE OF THE DS NP CHART BASED ON THE PERCENTILES OF THE RUN LENGTH DISTRIBUTION

The investigation of the percentiles of the RL distribution is useful in providing an in-depth understanding about the entire RL distribution of a control chart including the early false alarm rates. In this study, the percentiles of the RL distribution is calculated using (2.6). Table 2 displays the  $ARL$  and some of the percentiles of the RL distribution for the DS  $np$  chart with  $(n_1, n_2, WL, CL_1, CL_2) = (43, 2276, 1.5, 5.5, 34.5)$  when  $\delta_{opt} = 1.5$ ,  $n = 200$ ,  $p_0 = 0.01$  and  $MRL_{0\min} = 370.4$ .

The lower percentiles such as the 5th, 10th and 20th percentiles of the RL distribution for the in-control condition ( $\delta = 1$ ) provide information about the early false alarm rates. For example, the 10th percentile of the in-control RL

TABLE 1. Optimal parameters  $(n_1, n_2, WL, CL_1, CL_2)$  with the corresponding  $MRL_0$  and  $ARL_0$  for the DS  $np$  chart

| $\delta_{opt}$ | $p_0$ | $n$ | $MRL_{0min} = 200$ |       |      |        |        |         |         | $MRL_{0min} = 370.4$ |       |      |        |        |         |         |
|----------------|-------|-----|--------------------|-------|------|--------|--------|---------|---------|----------------------|-------|------|--------|--------|---------|---------|
|                |       |     | $n_1$              | $n_2$ | $WL$ | $CL_1$ | $CL_2$ | $MRL_0$ | $ARL_0$ | $n_1$                | $n_2$ | $WL$ | $CL_1$ | $CL_2$ | $MRL_0$ | $ARL_0$ |
| 1.5            | 0.005 | 100 | 8                  | 2340  | 0.5  | 2.5    | 17.5   | 205     | 294.82  | 47                   | 2285  | 1.5  | 3.5    | 18.5   | 375     | 541.15  |
|                |       | 200 | 74                 | 2366  | 1.5  | 4.5    | 19.5   | 212     | 305.13  | 63                   | 3430  | 1.5  | 5.5    | 26.5   | 374     | 539.64  |
|                |       | 400 | 103                | 3151  | 1.5  | 4.5    | 25.5   | 200     | 288.05  | 174                  | 3928  | 2.5  | 6.5    | 31.5   | 371     | 534.33  |
|                |       | 800 | 133                | 4650  | 1.5  | 6.5    | 35.5   | 200     | 288.80  | 320                  | 6127  | 3.5  | 11.5   | 46.5   | 371     | 534.51  |
|                | 0.01  | 50  | 4                  | 1167  | 0.5  | 2.5    | 17.5   | 209     | 301.69  | 25                   | 970   | 1.5  | 4.5    | 16.5   | 376     | 541.73  |
|                |       | 100 | 37                 | 1192  | 1.5  | 4.5    | 19.5   | 204     | 294.29  | 35                   | 1358  | 1.5  | 5.5    | 22.5   | 371     | 534.92  |
|                |       | 200 | 50                 | 1677  | 1.5  | 5.5    | 26.5   | 200     | 288.33  | 43                   | 2276  | 1.5  | 5.5    | 34.5   | 372     | 536.09  |
|                |       | 400 | 68                 | 2238  | 1.5  | 6.5    | 34.5   | 200     | 288.52  | 159                  | 3153  | 3.5  | 8.5    | 47.5   | 372     | 535.82  |
|                | 0.02  | 25  | 2                  | 580   | 0.5  | 2.5    | 17.5   | 221     | 318.03  | 11                   | 719   | 1.5  | 3.5    | 21.5   | 371     | 535.00  |
|                |       | 50  | 18                 | 646   | 1.5  | 4.5    | 20.5   | 201     | 290.36  | 16                   | 852   | 1.5  | 5.5    | 26.5   | 412     | 593.55  |
|                |       | 100 | 24                 | 921   | 1.5  | 4.5    | 28.5   | 218     | 313.94  | 41                   | 1214  | 2.5  | 7.5    | 36.5   | 373     | 538.18  |
|                |       | 200 | 32                 | 1254  | 1.5  | 5.5    | 37.5   | 206     | 296.28  | 106                  | 1512  | 4.5  | 9.5    | 46.5   | 376     | 541.67  |
|                | 0.005 | 100 | 23                 | 708   | 0.5  | 2.5    | 8.5    | 200     | 288.00  | 13                   | 1379  | 0.5  | 2.5    | 13.5   | 435     | 627.36  |
|                |       | 200 | 100                | 1115  | 1.5  | 4.5    | 12.5   | 224     | 323.27  | 104                  | 1002  | 1.5  | 4.5    | 12.5   | 376     | 542.84  |
|                |       | 400 | 226                | 1655  | 2.5  | 6.5    | 17.5   | 210     | 302.92  | 50                   | 1578  | 0.5  | 4.5    | 16.5   | 378     | 545.09  |
|                |       | 800 | 535                | 1995  | 4.5  | 10.5   | 22.5   | 208     | 300.42  | 768                  | 769   | 7.5  | 12.5   | 16.5   | 375     | 541.05  |
|                | 0.01  | 50  | 34                 | 352   | 1.5  | 4.5    | 8.5    | 202     | 291.78  | 8                    | 543   | 0.5  | 3.5    | 11.5   | 379     | 546.93  |
|                |       | 100 | 50                 | 559   | 1.5  | 4.5    | 12.5   | 226     | 325.44  | 13                   | 710   | 0.5  | 3.5    | 14.5   | 381     | 549.81  |
|                |       | 200 | 116                | 756   | 2.5  | 7.5    | 16.5   | 200     | 288.60  | 25                   | 787   | 0.5  | 4.5    | 16.5   | 394     | 568.76  |
|                |       | 400 | 268                | 994   | 4.5  | 9.5    | 22.5   | 200     | 288.96  | 384                  | 388   | 7.5  | 12.5   | 16.5   | 372     | 536.62  |
|                | 0.02  | 25  | 5                  | 208   | 0.5  | 2.5    | 9.5    | 264     | 381.12  | 4                    | 270   | 0.5  | 2.5    | 11.5   | 398     | 573.29  |
|                |       | 50  | 25                 | 282   | 1.5  | 4.5    | 12.5   | 224     | 323.19  | 26                   | 253   | 1.5  | 4.5    | 12.5   | 387     | 558.17  |
|                |       | 100 | 54                 | 494   | 2.5  | 5.5    | 19.5   | 201     | 289.68  | 9                    | 547   | 0.5  | 3.5    | 20.5   | 467     | 674.10  |
|                |       | 200 | 111                | 486   | 3.5  | 9.5    | 21.5   | 202     | 290.70  | 195                  | 297   | 8.5  | 11.5   | 19.5   | 434     | 626.06  |
|                | 0.005 | 100 | 84                 | 240   | 1.5  | 4.5    | 5.5    | 215     | 310.22  | 77                   | 406   | 1.5  | 3.5    | 7.5    | 374     | 539.79  |
|                |       | 200 | 184                | 252   | 2.5  | 4.5    | 7.5    | 203     | 293.03  | 182                  | 281   | 2.5  | 6.5    | 7.5    | 379     | 546.63  |
|                |       | 400 | 278                | 301   | 1.5  | 6.5    | 8.5    | 220     | 316.84  | 381                  | 438   | 4.5  | 7.5    | 11.5   | 490     | 707.18  |
|                |       | 800 | 534                | 534   | 2.5  | 8.5    | 13.5   | 263     | 379.19  | 425                  | 426   | 0.5  | 7.5    | 12.5   | 374     | 539.19  |
|                | 0.01  | 50  | 42                 | 120   | 1.5  | 4.5    | 5.5    | 220     | 317.61  | 16                   | 228   | 0.5  | 3.5    | 7.5    | 453     | 652.88  |
|                |       | 100 | 92                 | 127   | 2.5  | 4.5    | 7.5    | 209     | 300.76  | 91                   | 141   | 2.5  | 6.5    | 7.5    | 386     | 556.87  |
|                |       | 200 | 139                | 150   | 1.5  | 6.5    | 8.5    | 229     | 329.80  | 180                  | 186   | 3.5  | 7.5    | 10.5   | 450     | 648.66  |
|                |       | 400 | 237                | 238   | 1.5  | 7.5    | 13.5   | 221     | 318.30  | 212                  | 213   | 0.5  | 7.5    | 12.5   | 393     | 567.22  |
|                | 0.02  | 25  | 21                 | 61    | 1.5  | 4.5    | 5.5    | 221     | 318.83  | 8                    | 114   | 0.5  | 2.5    | 7.5    | 379     | 546.42  |
|                |       | 50  | 46                 | 64    | 2.5  | 4.5    | 7.5    | 222     | 319.85  | 37                   | 77    | 1.5  | 5.5    | 7.5    | 384     | 554.33  |
|                |       | 100 | 69                 | 77    | 1.5  | 6.5    | 8.5    | 230     | 331.92  | 64                   | 98    | 1.5  | 6.5    | 9.5    | 383     | 552.02  |
|                |       | 200 | 96                 | 121   | 0.5  | 6.5    | 13.5   | 209     | 301.60  | 105                  | 108   | 0.5  | 7.5    | 12.5   | 443     | 638.64  |

distribution is 57, indicating that there is a probability of 0.1 that a false alarm will occur by the 57th sample. On the other hand, it is about half of the time that a false alarm will occur by the 372nd sample, indicating that there is a probability of 0.5 that a false alarm will be detected by sample 372, while the  $ARL_0$  is given as 536.09.

The higher percentiles of the RL distribution for the out-of-control condition ( $\delta > 1$ ) provide information about the out-of-control that will be issued by the control chart at a certain magnitude of shift with a high probability. For example,



TABLE 2. ARLs and percentiles of the RL distribution for the DS  $np$  chart with  $(n_1, n_2, WL, CL_1, CL_2) = (43, 2276, 1.5, 5.5, 34.5)$  when  $\delta_{opt} = 1.5$ ,  $n = 200$ ,  $p_0 = 0.01$  and  $MRL_{0min} = 370.4$

| $\delta$ | $ARL$  | Percentiles of the run length distribution |     |      |      |      |      |      |      |      |      |      |      |      |  |
|----------|--------|--|-----|------|------|------|------|------|------|------|------|------|------|------|--|
|          |        | 1st  | 5th | 10th | 20th | 30th | 40th | 50th | 60th | 70th | 80th | 90th | 95th | 99th |  |
| 1.0      | 536.09 | 6  | 28  | 57   | 120  | 192  | 274  | 372  | 491  | 645  | 862  | 1234 | 1605 | 2467 |  |
| 1.1      | 161.29 | 2  | 9   | 17   | 36   | 58   | 83   | 112  | 148  | 194  | 259  | 371  | 482  | 741  |  |
| 1.2      | 63.39  | 1  | 4   | 7    | 15   | 23   | 33   | 44   | 58   | 76   | 102  | 145  | 189  | 290  |  |
| 1.3      | 30.91  | 1  | 2   | 4    | 7    | 11   | 16   | 22   | 28   | 37   | 49   | 71   | 92   | 141  |  |
| 1.4      | 17.93  | 1  | 1   | 2    | 4    | 7    | 9    | 13   | 16   | 21   | 29   | 41   | 53   | 81   |  |
| 1.5      | 11.93  | 1  | 1   | 2    | 3    | 5    | 6    | 8    | 11   | 14   | 19   | 27   | 35   | 53   |  |
| 2.0      | 4.80   | 1  | 1   | 1    | 1    | 2    | 3    | 3    | 4    | 6    | 7    | 10   | 13   | 20   |  |
| 3.0      | 2.69   | 1  | 1   | 1    | 1    | 1    | 2    | 2    | 2    | 3    | 4    | 5    | 7    | 10   |  |
| 4.0      | 1.93   | 1  | 1   | 1    | 1    | 1    | 1    | 1    | 2    | 2    | 3    | 4    | 5    | 7    |  |
| 5.0      | 1.56   | 1  | 1   | 1    | 1    | 1    | 1    | 1    | 1    | 2    | 2    | 3    | 3    | 5    |  |

the 90th percentile is 27 at  $\delta = 1.5$ , indicating that the DS  $np$  chart signals within the first 27 samples with a probability of 0.9.

It can be observed that the difference between the values of  $ARL_0$  and  $MRL_0$  is large when there is no shift ( $\delta = 1$ ) but this difference diminishes as the shift increases. This shows that the RL distribution can be highly skewed when there is no shift and the shape of the RL distribution changes with the magnitude of shift  $\delta$ .

## 6. CONCLUSIONS

In this study, the implementation of the MRL as a performance measure for the DS  $np$  chart has been studied and discussed. The optimal DS  $np$  chart is defined as the control chart with the smallest  $MRL_1$  value for a specified shift in the process fraction nonconforming, the desired  $ASS_0$  value and the desired  $MRL_0$  value. The MRL is a more suitable performance measure for the DS  $np$  chart compared to the ARL as the shape of the RL distribution changes in accordance to the shift in the process fraction nonconforming. The RL properties of the DS  $np$  chart are also furnished via the percentiles of the RL distribution in this study.

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